

LAYERED SAW NITROGEN DIOXIDE SENSOR BASED ON A ZnO/ 36° YX LiTaO₃ STRUCTURE WITH WO₃ SELECTIVE LAYER

S. J. Ippolito^{1,2}, K. Kalantar-Zadeh^{1,2}, A. Trinchì^{1,2}, W. Wlodarski^{1,2}, M. Tobar³

¹RMIT University, School of Electrical and Computer Systems Engineering, Melbourne, AUSTRALIA

²CRC for Micro-Technology, Hawthorn, VIC 3122, AUSTRALIA

³University of Western Australia, Department of Physics, AUSTRALIA

Abstract - A novel layered Surface Acoustic Wave (SAW) device is investigated for gas sensing of low levels NO₂ concentrations in air. The results show much higher sensitivity when compared against other SAW devices operating at the same frequency. The sensing structure is based on a layered SAW devices fabricated on a 36° X-cut, Y-propagating LiTaO₃ substrate. A ZnO guiding layer is employed to increase sensor sensitivity, whilst a thin film of WO₃ provides the selectivity towards NO₂. In this paper, the fabrication of the ZnO/36° YX LiTaO₃ sensor is described and micro-characterization of the selective layer is presented. Furthermore, a gas sensing experiment reveals the sensitivity of the device.

Keywords - Layered SAW, NO₂, Gas sensing, 36° YX LiTaO₃, ZnO

I. INTRODUCTION

Semiconductor metal oxide (SMO) films have been used extensively for toxic gas sensing. A sensor response using a metal oxide selective film is based upon sheet conductivity changes caused by interaction with gas molecules. Such changes in electrical conductivity have been noted since the earliest studies of semiconducting materials [1],[2]. Many reactions on the surface of metal oxides are possible which can be acceptable as the gas sensing mechanism. However, the most dominant reaction in semiconductor gas sensing is a reversible gas adsorption mechanism that occurs on the sensor's surface. The adsorbed gas atoms inject electrons into or extract electrons from the semiconducting material, depending on whether they are reducing or oxidizing respectively [3].

Nitrogen dioxide (NO₂), even at low ppm concentration levels, is hazardous for human health. Therefore, the development of sensors capable of measuring low concentrations of this gas is of significant importance. Tungsten trioxide (WO₃) films have been reported to show remarkable sensitive properties to NO₂ [4].

By the deposition of a SMO layer onto the active area of a SAW device, the device can be used for gas sensing applications. In a SAW device, the change in electrical conductivity perturbs the electro-acoustic properties of the underlying propagating acoustic wave. This results in the propagating acoustic wave changing its velocity. Deviations in velocity are monitored by measuring the changes in frequency or phase characteristics of the sensing device. Thus

the frequency or phase characteristics can be correlated to the corresponding concentration of the targeted gas exposed to the device.

Layered SAW transducers have shown significant attention in recent years for sensing applications [5],[6]. An increase in the confinement of acoustic energy at the surface of the device is made possible by using layered structures. The deposition of a piezoelectric guiding layer, such as zinc oxide (ZnO) generally results in further increasing the sensitivity of the device. ZnO is a piezoelectric material with a large electromechanical coupling coefficient [7]. The deposition of a ZnO layer onto the 36° XY LiTaO₃ substrate forms a layered SAW structure. Shoji et al. [8],[9] showed that deposition of ZnO layer onto 36° YX LiTaO₃ substrates results in an increased electromechanical coupling coefficient (K^2) for the SAW device. Prior to the deposition, a shear horizontal (SH) particle displacement with minimal normal component is the dominant acoustic wave propagation mode. After the deposition of the ZnO layer, SH displacement still retains. As a result, the sensor can operate in both gas and liquid media. The overall effect is the device having an enhanced sensitivity to perturbations caused by gas molecule interactions with the selective layer when compared to non-layered SAW device counterparts.

In this paper, a layered SAW structure based on ZnO/ 36° YX LiTaO₃ substrate is presented for NO₂ gas sensing applications. The design, fabrication and characterization of the deposited thin film are investigated. Finally, the response of the sensor to different NO₂ gas concentration is illustrated.

II. SENSOR FABRICATION

The sensor consisted of a two-port delay line with 64 input and output Inter Digital Transducer (IDT) finger pairs, 1.25mm aperture width and a periodicity of 24μm. The center-to-center distance between the IDTs was 85 wavelengths. The IDTs were formed by patterning a 2500Å aluminium layer and a 300Å layer of chromium. The aluminium layer was deposited upon the chromium to improved adhesion to the substrate.

Devices were fabricated with ZnO layer thickness of 1.2μm, deposited by an RF planar magnetron sputterer, using a

99.99% pure ZnO target. Sputtering gas was 40% O₂ in Ar and RF power was 120W, resulting in a deposition rate of ~1.2μm/hour.

The WO₃ selective layer was deposited by RF planar magnetron sputterer, using a 99.99% pure tungsten target. Using a mixture of 90% O₂ and 10% Ar, a deposition rate of approximately ~0.32μm per hour was achieved for 80W of the R.F. power. The sample was sputtered for duration of half an hour, resulting in a thickness of 0.16μm.

Both the ZnO and WO₃ were sputtered at a pressure of 1.0×10^{-2} Torr using the same substrate conditions of 260°C and at a distance of 6.5cm from the target.

III. MATERIAL ANALYSIS

The surface morphology of the ZnO film deposited onto a 36° YX LiTaO₂ substrate was characterized by Scanning Electron Microscopy (SEM) and the crystallinity by X-Ray Diffraction (XRD) analysis in pervious work [10]. Fig. 1 (a) shows the XRD pattern is seen of a 1.2μm layer of ZnO. The XRD pattern of the same structure with the addition of a 0.16μm layer of WO₃ deposited on top of the ZnO is shown in Fig. 1 (b).

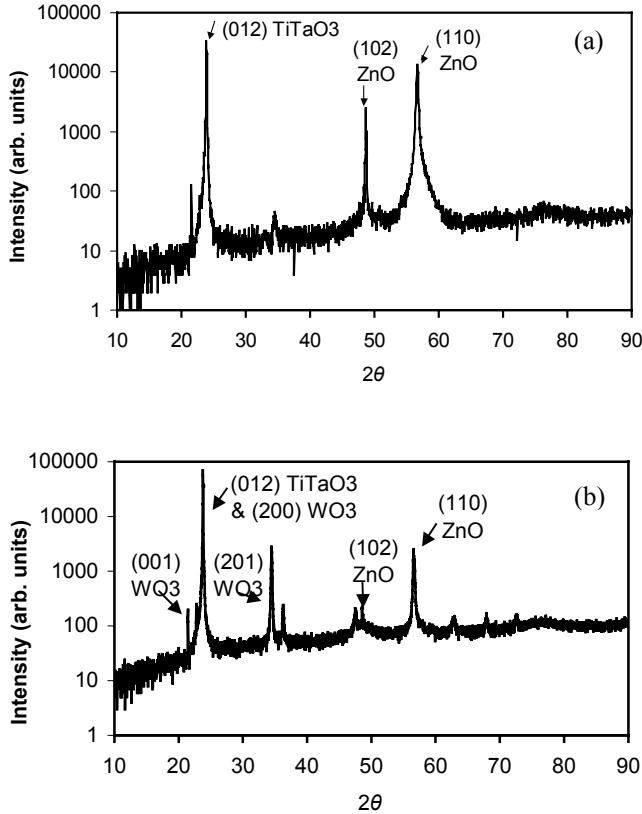


Fig 1. (a) XRD pattern of a 1.2μm layer of ZnO on LiTaO₃ substrate. (b) XRD XRD pattern of 750Å of WO₃ on a 1.2μm layer of ZnO on LiTaO₃ substrate.

From these results presented, a strong ZnO (110) peak indicates that the c-axis lies in the plane of the substrate. The presence of a smaller ZnO (102) peak is also seen, however, is dominated by the (110) peak [10]. XRD analysis of the sample with the WO₃ reveals the two peaks at angles of 2θ equaling 34.5° and 36.5°, respectively. At the position of the LiTaO₃ (012) main peak, it can be seen that the intensity of the peak is substantially increased. Cantalini and et al. [11] where able to show the existence of peak at 2θ equals 24 degrees when WO₃ is RF sputtered, which would suggest that the LiTaO₃ and WO₃ peaks overlap at this position. They also showed that a (201) peak at 2θ equals 34.5° correlates with WO₃ and that Al₂O₃ is represented by the peak at 2θ equals 36.5°. Hence, the same peak observed in Fig. 1 (b), where 2θ equals 36.5°, could be attributed to Al₂O₃ contamination during the WO₃ deposition.

IV. SENSITIVITY ANALYSIS

The theoretical change of the device's operational frequency, produced by the change in conductivity of the selective layer can be derived using perturbation theory, assuming weak coupling [6],

$$|\Delta f| = f \frac{K^2}{2} \frac{1}{1 + \left(\frac{V_o(\epsilon_s + \epsilon_A)}{\sigma \cdot d} \right)^2}, \quad (1)$$

where f is the operational frequency, Δf is the relative frequency change due to the conductivity change of the surface and K^2 is the electromechanical coupling coefficient. The variables that are a function of the deposited films are: V_o , the acoustic wave velocity that propagates in the substrate; σ , the bulk conductivity of the layer; and d defined as the layer thickness. The substrate and ambient atmospheric dielectric constants are ϵ_s and ϵ_A , respectively.

The decrease of the WO₃ film's conductivity is attributed to interaction with the NO₂, which is an oxidizing gas. As WO₃ is regarded as having a non-stoichiometric structure, free electrons originating from oxygen vacancies contribute to the conductivity of the thin film, outlined in (2),

$$O_{O(bulk)} = V_o + 2e' + \frac{1}{2}O_{2(gas)}, \quad (2)$$

where V_o is the vacancies and the $O_{O(bulk)}$ is present in the WO₃ layer. Due to the extra electron generated WO₃ is categorized an n-type semiconductor. Upon the introduction of the NO₂, it reacts with the WO₃ layer, decreasing the film's conductivity.

V. GAS SENSITIVITY ANALYSIS

The response of the sensor to low NO₂ concentrations (less than 1 ppb) levels in a balance of dry air is presented (Fig. 2). The sensor was placed in a computerized gas calibration system, where different concentrations of NO₂ gas was delivered via mass flow controllers. The operational temperature, linearity, recovery and response time were all analyzed and related to the NO₂ concentrations.

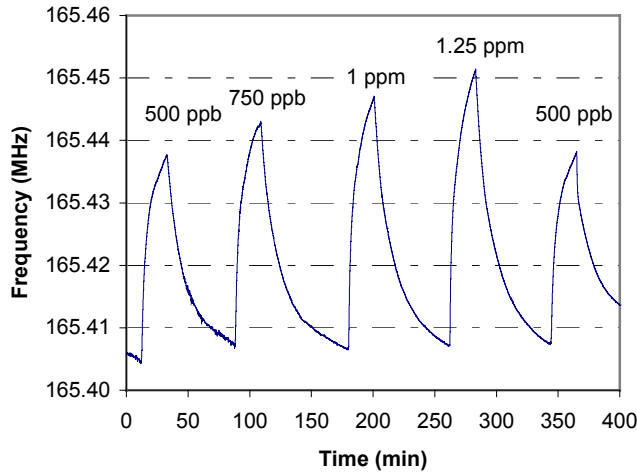


Fig. 2. Dynamic response of WO₃ based SAW sensor to different NO₂ concentrations at an operating temperature of 100°C and gas flow rate of 0.3 liters per minute.

The operational frequency of the device was approximately 165.406 MHz in air, at an operating temperature of around 100°C. At this operating temperature, preferred sensing characteristics (i.e. response repeatability to NO₂ concentrations) were observed. Additionally at 100°C, the maximum response was observed, yielding the highest frequency shift for a fixed concentration of NO₂, namely 1.25 ppm. It was found that linear increases in operational frequency were achieved by the introduction of NO₂, up to the saturation level of 1.5 ppm. Repeatability was also observed, when successive NO₂ pulses of 500 ppb were introduced to the sensor chamber. At this concentration a frequency shift of approximately 30 KHz was observed and is also presented in Fig. 2. The associated frequency shifts for 500ppb to 1.25ppm concentrations of NO₂ mixed with synthetic air are presented in Table 1.

TABLE I
FREQUENCY SHIFT VS NO₂ GAS CONCENTRATION

Nitrogen dioxide concentration	Shift in center frequency
1.25 ppm	43.86 kHz
1.00 ppm	39.45 kHz
750 ppb	35.62 kHz
500 ppb	30.22 kHz

Despite the large frequency shifts observed for such low concentrations, the sensor response times were long, and hence the gas exposure time was fixed at 20 minutes for each pulse of the analyte gas. The sensor returned to the same baseline frequency (165.406 MHz) following each NO₂ pulse, however the recovery time was approximately 58 minutes. It is believed that such long recovery times are due to the thickness of the WO₃ selective layer (0.16 µm). Tests are currently being conducted with thinner WO₃ layers in order to examine the effect of selective layer thickness against response and recovery times of the sensor. Furthermore, due to the limitations of the gas delivery equipment, responses to lower than 500 ppb concentrations of NO₂ were not able to be tested.

VI. CONCLUSION

The sensor response based on ZnO/ 36° YX LiTaO₃ structure was investigated for different concentrations of NO₂ gas in air. The operational frequency of the device was approximately 165 MHz. Linear increases in operational frequency are achieved by the introduction of NO₂, up to the saturation level of 1.5 ppm NO₂. A concentration of 500 ppb shows an approximate 30 KHz response.

Further investigations are planned where the optimal thickness of the selective layer will be studied. Furthermore, the effect of increasing the center frequency of the transducer will be tested in a bid to increase the sensitivity of the layered SAW device.

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